

Class Exercise 7 - The quasi-static approximation

Problem 1

Consider a ball with radius R and uniform charge Q . Find the force acting on the top half shell.

Solution

Recall from class that

$$\vec{F} = -\frac{1}{c^2} \frac{\partial}{\partial t} \iiint \vec{S} \, dV + \oiint \hat{T} \cdot d\vec{A},$$

where \hat{T} is the stress tensor, defined in Cartesian coordinates by

$$T_{ij} = \frac{1}{4\pi} \left(E_i E_j + B_i B_j - \frac{E^2 + B^2}{2} \delta_{ij} \right).$$

Since $\vec{B} = 0$ everywhere and the fields are static, we have $\vec{S} = 0$ and $\partial \vec{S} / \partial t = 0$. The electric field is (Gauss)

$$\vec{E}(r) = \begin{cases} \frac{Qr}{R^3} \hat{\mathbf{r}} & r < R \\ \frac{Q}{r^2} \hat{\mathbf{r}} & r \geq R \end{cases}$$

and since $\hat{\mathbf{r}} = \sin \theta \cos \varphi \hat{\mathbf{x}} + \sin \theta \sin \varphi \hat{\mathbf{y}} + \cos \theta \hat{\mathbf{z}}$ we have

$$T = \frac{1}{4\pi} \begin{pmatrix} E_x^2 - \frac{E^2}{2} & E_x E_y & E_x E_z \\ E_y E_x & E_y^2 - \frac{E^2}{2} & E_y E_z \\ E_z E_x & E_z E_y & E_z^2 - \frac{E^2}{2} \end{pmatrix}.$$

Due to symmetry in φ , the force can only be in the $\hat{\mathbf{z}}$ direction - every contribution from the bottom hemisphere at some $\varphi = \varphi_0$ has an opposite and equal contribution from the point $\varphi = -\varphi_0$, which cancel the contribution of the radial (the cylindrical radial coordinate) and angular directions. However, we have broken symmetry in the $\hat{\mathbf{z}}$ axis by only considering one of the hemispheres, so the contributions in $\hat{\mathbf{z}}$ do not cancel.

In total, we obtain an integral for the force in the form

$$F_z = \oint (T_{xz} dA_x + T_{yz} dA_y + T_{zz} dA_z),$$

where integration is done over the equator disk

$$A_{\text{disk}} = \left\{ r, \theta, \varphi : 0 \leq r \leq R, \theta = \frac{\pi}{2}, 0 \leq \varphi \leq 2\pi \right\},$$

$$d\vec{A}_{\text{disk}} = -r dr d\varphi \hat{z},$$

and the top “bowl”

$$A_{\text{bowl}} = \left\{ r, \theta, \varphi : r = R, 0 \leq \theta \leq \frac{\pi}{2}, 0 \leq \varphi \leq 2\pi \right\},$$

$$d\vec{A}_{\text{bowl}} = R^2 \sin \theta d\theta d\varphi \hat{r}.$$

We integrate and find

$$\begin{aligned} F_z^{(\text{bowl})} &= \frac{1}{4\pi} \int_0^{2\pi} \int_0^{\pi/2} R^2 \sin \theta d\theta d\varphi \left[E_x E_z \sin \theta \cos \varphi + E_y E_z \sin \theta \sin \varphi + \left(E_z^2 - \frac{E^2}{2} \right) \cos \theta \right] \\ &= \frac{R^2}{4\pi} \left(\frac{Q}{R^2} \right)^2 \int_0^{2\pi} \int_0^{\pi/2} \sin \theta \cos \theta d\theta d\varphi \left[(\sin \theta \cos \varphi)^2 + (\sin \theta \sin \varphi)^2 + \left(\cos^2 \theta - \frac{1}{2} \right) \right] \\ &= \frac{Q^2}{2R^2} \int_0^{\pi/2} \sin \theta \cos \theta d\theta \left(\sin^2 \theta + \cos^2 \theta - \frac{1}{2} \right) \\ &= \frac{Q^2}{4R^2} \int_0^{\pi/2} \sin \theta \cos \theta d\theta = \frac{Q^2}{8R^2} \int_0^{\pi/2} \sin 2\theta d\theta = \frac{Q^2}{8R^2}, \end{aligned}$$

$$\begin{aligned} F_z^{(\text{disk})} &= -\frac{1}{4\pi} \iint \left(E_z^2 - \frac{E^2}{2} \right) dA_z \\ &= -\frac{1}{4\pi} \int_0^{2\pi} \int_0^R r dr d\varphi \left(E_z^2 - \frac{E^2}{2} \right) \\ &= -\frac{Q^2}{4\pi} \int_0^{2\pi} \int_0^R r dr d\varphi \frac{r^2}{R^6} \left(\cos^2 \left(\frac{\pi}{2} \right) - \frac{1}{2} \right) \\ &= \frac{Q^2}{16R^2}, \end{aligned}$$

which gives a total force

$$\vec{F}_{\text{tot}} = \frac{3Q^2}{16R^2} \hat{z}.$$

Problem 2

An electric field with frequency ω propagates along the axis of a conducting cylinder with conductivity σ . Describe the electric field in the conductor in the quasi-static approximation.

Solution

Before using the quasi-static approximation, we combine the pair of Maxwell equations

$$\vec{\nabla} \times \vec{B} = \frac{4\pi}{c} \vec{J} + \frac{1}{c} \frac{\partial \vec{E}}{\partial t},$$

and

$$\vec{\nabla} \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{B}}{\partial t},$$

into a single differential equation for \vec{E} . We take the rotor of the second equation and insert into it the first one,

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{E}) = -\frac{1}{c} \frac{\partial}{\partial t} (\vec{\nabla} \times \vec{B}) = -\frac{4\pi\sigma}{c^2} \frac{\partial \vec{E}}{\partial t} - \frac{1}{c^2} \frac{\partial^2 \vec{E}}{\partial t^2},$$

where we used the relation $\vec{J} = \sigma \vec{E}$. Neglecting the charge density (due to super fast decay in the large σ limit), we can use

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{E}) = \vec{\nabla} \left(\underbrace{\vec{\nabla} \cdot \vec{E}}_{=0} \right) - \nabla^2 \vec{E},$$

and therefore we have

$$\nabla^2 \vec{E} = \frac{4\pi\sigma}{c^2} \frac{\partial \vec{E}}{\partial t} + \frac{1}{c^2} \frac{\partial^2 \vec{E}}{\partial t^2}.$$

Assuming $\vec{E} \propto e^{-i\omega t} \hat{\epsilon}$, we find

$$\nabla^2 \vec{E} = \left(-\frac{4\pi i\omega\sigma}{c^2} - \frac{\omega^2}{c^2} \right) \vec{E}.$$

Now we apply the quasi-static approximation $\sigma \gg \omega$, and find that the second term is negligible. In cylindrical coordinates we find

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \vec{E}}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \vec{E}}{\partial \theta^2} + \frac{\partial^2 \vec{E}}{\partial z^2} = -\frac{4\pi i\omega\sigma}{c^2} \vec{E}.$$

As usual, we look for solutions of the form

$$E(\vec{r}) = R(r) e^{im\theta} e^{ikz},$$

where the full solution will be $E(\vec{r}) e^{-i\omega t}$. Inserting this form into the above equation gives a Bessel equation,

$$\frac{\partial^2 R(r)}{\partial r^2} + \frac{1}{r} \frac{\partial R(r)}{\partial r} + \left(\left(\sqrt{\frac{4\pi i\omega\sigma}{c^2} - k^2} \right)^2 - \frac{m^2}{r^2} \right) R(r) = 0.$$

The only solution which does not diverge at $r = 0$ is a Bessel function of the first kind, and therefore inside the cylinder we have

$$E(\vec{r}, t) = e^{-i\omega t} \sum_{m,k} A_{m,k} J_m \left(r \sqrt{\frac{4\pi i\omega\sigma}{c^2} - k^2} \right) e^{im\theta} e^{ikz}.$$

For simplicity, we consider now a cylinder with complete rotational and translational symmetries, such that the problem is independent of both z and θ . Therefore, we focus on the $m = k = 0$ modes, for which the solution becomes

$$E(\vec{r}, t) \propto J_0 \left(\sqrt{\frac{4\pi i\omega\sigma}{c^2}} r \right) e^{-i\omega t}.$$

For $(r\sqrt{\sigma\omega}/c) \gg 1$, the dominant contribution from the Bessel function J_0 is

$$J_0(s \gg 1) \sim e^{is} \implies J_0 \left(\sqrt{\frac{4\pi i\omega\sigma}{c^2}} r \right) \sim \exp \left(i \sqrt{\frac{4\pi i\omega\sigma}{c^2}} r \right).$$

Recall that $\sqrt{i} = (1+i)/\sqrt{2}$, and thus

$$J_0 \left(\sqrt{\frac{4\pi i\omega\sigma}{c^2}} r \right) \sim \exp \left(i \frac{(1+i)}{c} \sqrt{2\pi\omega\sigma} r \right) = \underbrace{\exp \left(i \frac{\sqrt{2\pi\omega\sigma}}{c} r \right)}_{\text{oscillatory}} \underbrace{\exp \left(-\frac{\sqrt{2\pi\omega\sigma}}{c} r \right)}_{\text{decaying}},$$

which means the field decays inside the conductor! Notice that as ω or σ grow, the decay gets prominent at increasingly short distances. At the limit of infinite conductivity the field inside the conductor vanishes completely.

Problem 3

An infinitely long metal cylinder with radius a , conductivity σ and magnetic permeability μ is coaxial with an infinite solenoid of radius $b > a$ and n turns per unit length, which carries a current $I = I_0 e^{-i\omega t}$. Find the magnetic and electric fields everywhere in the quasi-static approximation.

Solution

The system is symmetric with respect to the axis of the cylinder (which we choose to be $\hat{\mathbf{z}}$), and the only variation of the current is in time. The primary magnetic field H_0 , due to the solenoid, is therefore uniform in space and directed along the axis of symmetry. In turn, H_0 will induce an electric field on the cylinder (Faraday's),

$$\oint \vec{E} \cdot d\vec{\ell} = -\frac{1}{c} \frac{\partial}{\partial t} \int \vec{B} \cdot d\vec{S},$$

producing, in turn, currents in the $\hat{\boldsymbol{\theta}}$ direction all along the cylinder, since

$$\vec{J} = \sigma \vec{E} = \sigma E_{\theta} \hat{\boldsymbol{\theta}}.$$

We find that the solenoid has induced a current configuration (termed *eddy currents*) which look like many additional coaxial solenoids inside the cylinder!

The “inner solenoids” contribute only to the magnetic field inside the cylinder, since outside a solenoid the magnetic field is zero. Thus, the total magnetic field outside the cylinder is $H_0 = B_0/\mu = nI_0 e^{-i\omega t}$, while inside it is given by the solution to

$$\nabla^2 H = \frac{4\pi\mu\sigma}{c^2} \frac{\partial H}{\partial t},$$

gotten by using the quasi-static approximation of $\partial E/\partial t \propto \omega E \ll \sigma E$ in the Maxwell equations

$$\vec{\nabla} \times \vec{B} = \frac{4\pi\mu}{c} \vec{J} + \frac{1}{c} \frac{\partial \vec{E}}{\partial t},$$

and

$$\vec{\nabla} \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{B}}{\partial t}.$$

We know that the magnetic field will only be in the $\hat{\mathbf{z}}$ direction, and due to symmetry there will be no dependence on θ and z . Therefore, we obtain a Bessel equation for H in the form

$$\left[\frac{d^2}{dr^2} + \frac{1}{r} \frac{d}{dr} + k^2 \right] H = 0,$$

where

$$k = \frac{1+i}{\delta}, \quad \delta = \frac{c}{(2\pi\mu\sigma\omega)^{1/2}}, \quad H = H_z(r) e^{-i\omega t}, \quad H_\theta = H_r = 0.$$

The boundary condition at $r = a$ is $H(a) = H_0$, so the only finite (for $r \rightarrow 0$) solution is

$$H = H_0 \frac{J_0(kr)}{J_0(ka)},$$

where $J_0(kr)$ is the zero-order Bessel function of the first kind. Outside the cylinder we have $H(a \leq r \leq b) = H_0$ and $H(r > b) = 0$. We find the electric field inside the cylinder using Faraday's law,

$$\begin{aligned} \oint \vec{E} \cdot d\vec{\ell} &= -\frac{1}{c} \frac{\partial}{\partial t} \int \vec{B} \cdot d\vec{S} = -\frac{\mu}{c} \frac{\partial}{\partial t} \int \vec{H} \cdot d\vec{S} \\ \implies 2\pi r E_\theta &= \frac{2\pi\mu i\omega H_0 e^{-i\omega t}}{c} \frac{H_0 e^{-i\omega t}}{J_0(ka)} \int_0^r J_0(kr') r' dr' \end{aligned}$$

We use the integral identity for Bessel functions

$$\int x^p J_{p-1}(x) dx = x^p J_p(x) + c,$$

to obtain

$$\int_0^r J_0(kr') r' dr' = \frac{1}{k^2} [kr J_1(kr) - (k \cdot 0) J_1(0)] = \frac{r}{k} J_1(kr),$$

where we have used the fact that $J_{n>0}(0) = 0$. The electric field inside the cylinder is then

$$\begin{aligned} 2\pi r E_\theta &= \frac{2\pi\mu i\omega H_0 e^{-i\omega t}}{ck} \frac{r J_1(kr)}{J_0(ka)} \\ \implies E_\theta(r < a) &= \frac{i\omega\mu H_0 e^{-i\omega t}}{ck} \frac{J_1(kr)}{J_0(ka)}. \end{aligned}$$

The current density is then given by

$$J_\theta = \frac{i\omega\mu H_0 e^{-i\omega t}}{\sigma ck} \frac{J_1(kr)}{J_0(ka)}, \quad J_r = J_z = 0.$$

To determine the electric field outside the cylinder we use Faraday's law once more, and find

$$\begin{aligned}
 \oint \vec{E} \cdot d\vec{\ell} &= -\frac{\mu}{c} \frac{\partial}{\partial t} \int \vec{H}_{\text{tot}} \cdot d\vec{S} \\
 \Rightarrow E_{\theta} &= \frac{2\pi}{2\pi r} \frac{i\mu\omega}{c} e^{-i\omega t} \int_0^r \left[H_0 \frac{J_0(kr')}{J_0(ka)} \Theta(a-r') + H_0 [\Theta(b-r') - \Theta(a-r')] \right] r' dr' \\
 \Rightarrow E_{\theta}(a \leq r \leq b) &= \left[\frac{i\mu\omega a H_0}{crk} \frac{J_1(ka)}{J_0(ka)} + \frac{i\mu\omega H_0}{cr} (r^2 - a^2) \right] e^{-i\omega t}, \\
 \Rightarrow E_{\theta}(r > b) &= \left[\frac{i\mu\omega a H_0}{crk} \frac{J_1(ka)}{J_0(ka)} + \frac{i\mu\omega H_0}{cr} (b^2 - a^2) \right] e^{-i\omega t}.
 \end{aligned}$$